

Goal

Benchmarking three different **solutions** to drive directly (i.e. **without gearbox**) the shedding mechanism of the **weaving looms** applications, which have a strongly oscillating load pattern; the **solutions** are:

- 1) conventional PM synchronous motor (**EM1**)
- 2) conventional PM synchronous motor with assistance of a **separate magnetic spring** (**EM2MS**)
- 3) PM synchronous motor with assistance of **integrated magnetic spring** (**EMMS**)

The main performance **indicators** for the benchmarking of this study are the amount of required **materials**, the **consumed power** and the **flexibility**.

Motivation

- Electric motor systems consume a large part of the generated energy which is about **46%** of the generated energy worldwide [ref1]. Reducing energy consumption is crucial. This work focuses on applications with cyclic load pattern.
- Recently, **passive** elements such as **magnetic** and **mechanical springs** have received interest for applications with a cyclic load pattern. The main goal of using these passive elements is to store energy and release it when needed.
- In [ref2], a **comparison** between the **energy** consumption of a permanent magnet motor **with** and **without magnetic spring** for high dynamic industrial applications was reported. It was found that energy consumption and peak torque of the magnetic spring assisted drivetrain are about **6** and **3** times respectively **lower** than using the conventional servo motor.
- A disadvantage of **the spring** is that its torque profile is fixed by **design** of the spring, which reduces the **flexibility** of the drive system towards other load patterns.

Approach

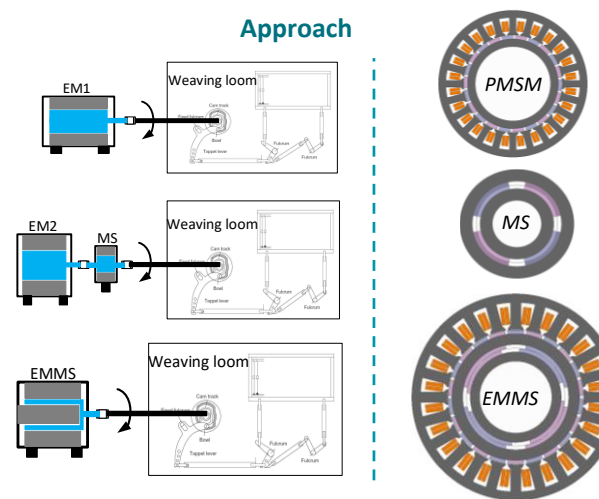


Fig. 1. Schematic of the three drivetrains.

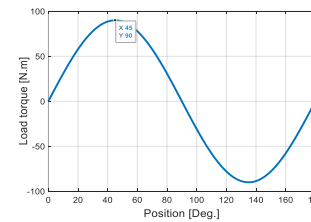


Fig. 2. Load torque versus the rotating position at 600 rpm.

Table I. Design parameters

- (1) Shaft radius
- (2) Inner stator yoke thickness
- (3) PM coverage ratio of the magnetic spring
- (4) PM thickness of the magnetic spring
- (5) Rotor yoke thickness
- (6) PM coverage ratio of the motor
- (7) PM thickness of the motor
- (8) Teeth width
- (9) Teeth height
- (10) Stator yoke thickness
- (11) Stack length

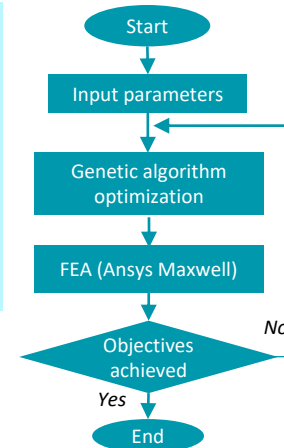
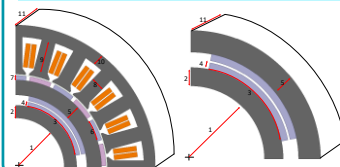


Fig. 3. Optimization flow chart.

Results

Parameter	EM1	EM2+MS	EMMS
Outer diameter [mm]	192	192+116	192
Stack length [mm]	110	65+80	75
Steel mass [Kg]	9.60	5.65+3 =8.65	8.50
Copper mass [Kg]	2.40	1.45	1.60
Magnet mass [Kg]	0.95	0.55+0.75=1.30	1.30
Total mass [Kg]	12.95	11.40	11.40
Motor RMS torque [N.m]	63	33	33
Inertia [Kg.m ²]	0.010	0.0062+0.0032 =0.0094	0.011
Total losses [W]	178	89+22=111	121
Flexibility	High	Medium	Low
Cost	low	Medium	High

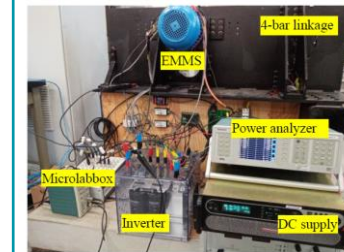


Fig. 4. Experimental setup.

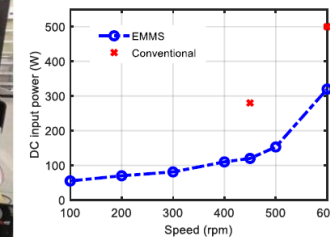


Fig. 5. Measured DC input power

Key take-aways

- The power consumption of the drivetrains that use a **magnetic spring** is **lower** by about **40%** compared to the **conventional electric motor**.
- Introducing a **magnetic spring** in the drivetrain **reduces** the **flexibility** of the system.
- The **cost** of the **magnetic spring** assisted drivetrain is **higher**. However, the higher cost of the drivetrain will be paid back by **lower energy consumption**.

Further reading

- ref1: <https://doi.org/10.1109/MIAS.2010.939427>
- ref2: <https://doi.org/10.3390/act8010018>