1 Stem hydraulic capacitance decreases with drought stress: implications for modelling tree

2 hydraulics in the Mediterranean oak *Quercus ilex*

- 3 Running title: Seasonality in stem hydraulic capacitance
- 4 Salomón, Roberto L^{1,2}; Limousin, Jean Marc³; Ourcival, Jean Marc³; Rodríguez-Calcerrada, Jesús¹;

5 Steppe, Kathy²

- 6 ¹ Forest Genetics and Ecophysiology Research Group, E.T.S. Forestry Engineering, Technical
- 7 University of Madrid, Ciudad Universitaria s/n, 28040, Madrid, Spain
- 8 ² Laboratory of Plant Ecology, Department of Applied Ecology and Environmental Biology, Faculty of
- 9 Bioscience Engineering, Ghent University, Coupure links 653, B-9000 Ghent, Belgium
- ³ Centre d'Ecologie Fonctionnelle et Evolutive CEFE, CNRS, UMR 5175, 1919 route de Mende, F-34293
- 11 Montpellier, Cedex 5, France
- 12 Corresponding author: Salomón, Roberto L.; email address:
- 13 RobertoLuis.SalomonMoreno@UGent.be

14 Abstract

15 Hydraulic modelling is a primary tool to predict plant performance in future drier scenarios. 16 However, as most tree models are validated under non-stress conditions they may fail when water 17 becomes limiting. To simulate tree hydraulic functioning under moist and dry conditions, the current 18 version of a water flow and storage mechanistic model was further developed by implementing 19 equations that describe variation in xylem hydraulic resistance (R_x) and stem hydraulic capacitance 20 (C_s) with predawn water potential (Ψ_{PD}). The model was applied in a Mediterranean forest 21 experiencing intense summer drought, where six Quercus ilex trees were instrumented to monitor 22 stem diameter variations and sap flow, concurrently with measurements of predawn and midday leaf water potential. Best model performance was observed when Cs was allowed to decrease with 23 decreasing Ψ_{PD} . Hydraulic capacitance decreased from 62 to 25 kg m⁻³ MPa⁻¹ across the growing 24 25 season. In parallel, tree transpiration decreased to a greater extent than the capacitive water release and the contribution of stored water to transpiration increased from 2.0% to 5.1%. Our results 26 27 demonstrate the importance of stored water and seasonality in C_s for tree hydraulic functioning, and they suggest that C_s should be considered to predict the drought-response of trees with models. 28

Keywords: radial stem growth, drought, hydraulic conductance, process-based modelling, holm oak,
stem water storage, hydraulic function

32 1 Introduction

33 As soil dries and atmospheric vapor pressure deficit intensifies, xylem conduits are subjected to 34 lower water potential and may eventually cavitate, thus limiting tree water transport. Xylem 35 vulnerability to drought-induced cavitation has been measured in hundreds of species as the main 36 attribute to quantify tree resistance to drought (Choat et al., 2012; Sperry & Love, 2015). A growing 37 body of evidence points, however, to a complementary factor involved in drought resistance: the 38 radial water flow in stems to maintain tree hydraulic integrity by buffering changes in xylem water 39 potential and limiting cavitation of xylem conduits (Goldstein et al., 1998; Meinzer et al., 2003; Steppe & Lemeur, 2004; Scholz et al., 2007; Steppe et al., 2012; McCulloh et al., 2014). In this way, 40 41 plant tolerance to drought does not solely rely on inherent xylem resistance to cavitation, but also on 42 the radial capacitive release of stored water from elastic-living tissues that transiently reduces xylem tension at a given rate of flow and hence cavitation. Accordingly, a trade-off between hydraulic 43 44 capacitance and structural traits involved in xylem resistance to cavitation has been observed across 45 a wide range of woody species (Meinzer et al., 2008, 2009). Nevertheless, the role of hydraulic 46 capacitance in plant hydraulics has been traditionally overshadowed by the study of drought-induced 47 cavitation and the vulnerability of xylem to changes in water potential (Meinzer et al., 2009; 48 McCulloh et al., 2014; Epila et al., 2017).

49 Hydraulic modelling is a key tool to mechanistically understand how trees cope with severe and intense drought events (Mencuccini et al., 2015; Steppe et al., 2015a). Mechanistic models 50 51 developed for well-watered conditions commonly use static parameters to describe constant xylem 52 hydraulic conductance (Steppe et al., 2006, 2008a; Verbeeck et al., 2007; Zweifel et al., 2007; De 53 Schepper & Steppe, 2010), whereas variable hydraulic conductance as a function of water potential 54 has been successfully implemented as the soil dries out (Sperry et al., 1998; Baert et al., 2015; 55 Mencuccini et al., 2015). Likewise, static parameters are used to describe hydraulic capacitance (e.g. Sperry et al., 1998; Steppe et al., 2006; Zweifel et al., 2007; Baert et al., 2015); however, none of 56 57 these models consider the variability in stem hydraulic capacitance, although stem water reservoirs

are progressively depleted under dry conditions (Scholz *et al.*, 2007, 2008; Verbeeck *et al.*, 2007;
Betsch *et al.*, 2011; Kocher *et al.*, 2013; Matheny *et al.*, 2015). Accounting for the dynamic drought
response of both hydraulic conductance and capacitance could improve model performance under a
wide range of environmental conditions and extended time frames (Steppe *et al.*, 2008b). Model
refinement via integration of tree drought responses has therefore been encouraged to advance in
our mechanistic understanding of tree hydraulic functioning in future drier scenarios (Verbeeck *et al.*,
2007; Baert *et al.*, 2015; Mencuccini *et al.*, 2015; Steppe *et al.*, 2015a, 2015b).

65 In this study, we aimed at modelling tree hydraulic functioning in field-grown Quercus ilex L. under wet to dry conditions by taking into account the dynamic nature of both xylem resistance to water 66 67 transport (R_x) and stem hydraulic capacitance (C_s) . For this purpose, process-level equations that describe the relationship of R_x and C_s with predawn water potential (Ψ_{PD}) have been implemented in 68 the current version of a sophisticated mechanistic model that integrates tree water transport 69 70 dynamics and stem diameter variations (Steppe et al., 2006, 2008a; De Swaef et al., 2015). Water 71 reservoirs are defined here as the elastic tissues subjected to reversible diel cycles of water release 72 and refill to avoid xylem cavitation. Inelastic water release from cavitated xylem conduits under 73 negative water potential (Tyree & Ewers, 1991; Hölttä et al., 2009) is neglected because the rapid 74 reversibility of this phenomenon remains a matter of debate (Brodersen & McElrone, 2013; Cochard 75 & Delzon, 2013). An advantage of this approach is that measurements are not destructive, since the 76 model is driven by sap flow and Ψ_{PD} , and calibrated against stem diameter variations and xylem 77 water potential at midday. As these variables can be monitored with peripheral devices and by 78 sampling a small number of leaves, the hydraulic functioning of surveyed trees can be continuously 79 modelled and research is not restricted to discrete observations.

We hypothesize that including daily variations in R_x and C_s as a function of Ψ_{PD} improves model accuracy in predicting stem diameter variations and xylem water potential during the dry season. Contrarily, we predict that variability in R_x and C_s may not improve model performance during the wet season as R_x and C_s are expected to remain constant. The integrated root-to-leaf R_x was

modelled as function of Ψ_{PD} using a negative exponential curve (Baert *et al.*, 2015), an alternative 84 approach to estimate the integrated root-to-leaf hydraulic conductance ($K_x = 1/R_x$) and generate 85 vulnerability curves. Furthermore, a new equation defining the relationship between C_s and Ψ_{PD} was 86 developed using the shape of water desorption curves and cumulative water release curves reported 87 88 for several species (Zweifel et al., 2000; Meinzer et al., 2003, 2009; Steppe et al., 2006; Barnard et al., 2011; McCulloh et al., 2014). Both magnitude of the decrease in Cs during the dry season and 89 90 contribution of stored water to the transpiration stream were evaluated. Simulated cumulative water 91 release from internal storage pools was compared with estimates of stem water refilling at the end 92 of the dry season after first autumn heavy rains. Likewise, the simulated vulnerability curve was 93 compared to the vulnerability curves obtained by measurements at the organ scale in the same 94 experimental site (Limousin et al., 2010a; Martin-StPaul et al., 2014).

95 2 Materials and methods

96 2.1 Site description

97 The study site is located in the Puéchabon State Forest (Montpellier, France) in a stand dominated by 98 Q. ilex (43°44'29" N, 3°35'45" E, 270 m.a.s.l.). The stand has been historically subjected to periodic 99 coppicing, with the last cut being performed in 1942. Nowadays, top canopy height is 5.5 m, stand 100 density is 4700 stems ha⁻¹, and most stems (> 70%) range in diameter at breast height (DBH) from 4 101 to 10 cm. Buxus sempervirens L., Phyllirea latifolia L., Pistacia terebinthus L. and Juniperus oxycedrus 102 L. are the main species of the understory layer. The area has a Mediterranean-type climate: annual 103 mean temperature is 13.4 °C, annual precipitation is 907 mm, and 80% of this amount falls during 104 winter and autumn, when temperatures are lower (Limousin et al., 2009). A weather station located 105 at the experimental site was used to monitor meteorological conditions. Air temperature, relative 106 humidity (MP100, Rotronic, Bassersdorf, Switzerland), and rainfall (tipping bucket rain gauge 107 ARG100, Environmental Measurements Ltd, Sunderland, UK) were measured every minute and averaged every 30 minutes with a data logger (model 21X, Campbell Scientific Ltd, Shepshed, UK).
More details on the experimental site are available in Rambal *et al.* (2014).

110 **2.2 Tree and soil measurements**

Six *Q. ilex* trees (see Table 1) were instrumented to continuously monitor sap flow and stem diameter variations. We selected data from the year 2009 because it was characterized by a strong and typical summer drought between mid-July and mid-September, and due to data availability on leaf water potential at predawn and midday in the instrumented trees during the summer.

Sap flux density (g cm⁻² h⁻¹) was continuously monitored with thermal dissipation probes (Granier, 115 116 1985). Probe pairs were inserted at 1.2 m height with a vertical separation of 10 cm. Probes were 117 oriented facing north to avoid direct solar heating, and were protected from rain and radiation by 118 aluminum cover. Temperature difference between the probes was registered every 5 minutes, and 119 averaged and recorded every 30 minutes with a data logger (model CR10X, Campbell Scientific). Sap 120 flux density was calculated considering zero flow from the absolute maximum temperature 121 difference over 2-day running periods. Sap flux density was upscaled to the tree level to obtain sap flow (F_{STEM} , g h^{-1}) by multiplying sap flux density by sapwood area. Sapwood area was estimated from 122 123 an allometric relationship between tree DBH and sapwood area obtained from 18 additional trees (Limousin et al., 2009). For further details about F_{STEM} measurements see Limousin et al. (2009). 124

Stem circumference variations were recorded using automatic band dendrometers (ELPA-98, University of Oulu, Oulu, Finland). Dendrometers were just below the thermal dissipation probes, and the outer layer of dead bark was removed prior to installation. Circumference variations were registered every 5 minutes and recorded every 30 minutes with a data logger (model CR1000; Campbell Scientific Ltd, Shepshed, UK) and transformed to stem diameter variations (ΔD , μm). For further details about ΔD measurements see Lempereur et al. (2015).

131 Leaf water potential (Ψ_{LEAF} , MPa) was measured with a pressure chamber (PMS1000, PMS 132 Instruments, Corvallis, OR, USA) on DOYs 114, 176, 208, 234 and 310 during the 2009 growing season

133 (23 April, 24 June, 26 July, 21 August, 5 November, respectively) at predawn (before 06:00 h) and 134 midday (14:00 h). Two leaves were sampled per tree and a third leaf was sampled if the observed 135 difference between measurements was higher than 0.2 MPa. Samples were taken at similar tree 136 heights and measurements were performed within 1 min after leaf excision. Leaf water potential was 137 measured in four of the six trees instrumented for F_{STEM} and ΔD measurements. Average Ψ_{LEAF} of 138 these four trees was used for the two remaining trees.

139 The discrete measurements of Ψ_{PD} were interpolated on a daily basis using modelled soil water 140 storage (SWS, mm). Daily soil water storage was modelled using the soil water balance module of the 141 SIERRA vegetation model driven by daily values of solar radiation, minimum and maximum temperature and precipitation (Mouillot *et al.*, 2001; Ruffault *et al.*, 2013). Soil water storage and Ψ_{PD} 142 143 were related by a Campbell-type retention curve (Campbell, 1974). The soil water storage model was 144 validated against measurements of SWS integrated over a rooting depth of 4.5 m and performed at 145 approximately monthly intervals from 1998 to 2009 using a neutron moisture gauge (see Rambal et al. 2003 for further details). The relationship between modelled and measured SWS displayed a good 146 agreement ($R^2 = 0.92$; p < 0.0001; RMSE = 16 mm; n = 90), as well as the relationship between 147 modelled and measured Ψ_{PD} (R² = 0.73; p < 0.0001; RMSE = 0.71 MPa; n = 95). Despite the good fit 148 149 obtained between SWS and Ψ_{PD} on an annual basis, Ψ_{PD} was underestimated by the soil water 150 balance model during summer drought. To correct daily simulated values of Ψ_{PD} in summer, 151 optimized parameters for each tree were selected to account for spatial heterogeneity in leaf area 152 index, soil texture and stone fraction.

153 2.3 Mechanistic tree modelling

154 **2.3.1 Model description**

The current version of a mechanistic water flow and storage model (Steppe *et al.*, 2008a) was used to study the hydraulic functioning of *Q. ilex* trees. Briefly, the model is composed of two interconnected sub-models describing dynamics in tree water transport and stem diameter variations, in which F_{STEM} 158 dynamics are intimately linked to stem ΔD by radial water flow between the xylem and the outer tissues. Note that "stem" refers to the tree trunk, so that branches are excluded for model simplicity. 159 160 The model assumes the xylem as a rigid cylinder (xylem compartment) surrounded by an elastic outer ring composed of cells of cambium, phloem and bark (storage compartment) responsible for diel 161 162 shrinkage and swelling (Steppe et al., 2006). Therefore, the water stored in outer elastic cells 163 constitutes the only capacitive water source; water release from the xylem parenchyma and cavitated conduits is neglected by this model. Sap flow (F_{STEM}) integrates the axial water flow through the xylem 164 compartment via root water uptake (fx) and the radial water exchange between xylem and storage 165 166 compartment (f_s). Axial water flow (f_x) is calculated as the water potential gradient between the roots and the stem divided by R_x, and radial water flow (f_s) is calculated as the first derivative defining the 167 168 change in water content of the storage compartment, which is influenced by the resistance to radial flow between xylem and storage compartment (R_s , MPa h g^{-1}). The model equations are shown in the 169 supplementary material (Note S1). When transpiration starts, a water potential gradient between 170 171 xylem and storage compartment ($\Psi_x - \Psi_s$) leads to radial flow from outer cells to the xylem to fulfill 172 the transpiration need; Ψ_X is inferred from Ψ_{LEAF} measurements (see below), whereas Ψ_S is estimated 173 as a function of the water content and capacitance of the storage compartment (see Note S1). Water 174 depletion in the morning results in reduction in cell turgor and reversible stem shrinkage. Conversely, 175 water refilling in the afternoon, when atmospheric vapor pressure deficit and transpiration start to 176 decline, results in reversible stem swelling. Water potential in the storage compartment is the algebraic sum of the osmotic potential (Ψ_s^{O}) and the turgor pressure (Ψ_s^{P}). Irreversible stem growth 177 178 occurs when carbon requirements are met (Daudet et al., 2005) and turgor pressure exceeds a 179 threshold value for cell wall yielding (Γ , Lockhart 1965). For a detailed explanation of the principles of the model see Steppe et al. (2006, 2008a) and De Pauw et al. (2008). 180

To allow variation in xylem hydraulic resistance of the root-to-leaf continuum (R_x , MPa h g⁻¹) and stem hydraulic capacitance (C_s , g MPa⁻¹), the model was further developed by implementing two equations and their corresponding parameters:

184 The hydraulic resistance was described to vary exponentially with Ψ_{PD} (Baert *et al.*, 2015), which 185 accounted for day to day variations in R_X with soil drying while assuming no daily refilling of cavitated 186 xylem:

187
$$R_X = r_1 e^{(\Psi_{PD}^2) r_2}$$
 Eqn. 1

188 where r_1 (MPa h g⁻¹) and r_2 (MPa⁻²) are the proportionality parameters influenced by plant 189 characteristics.

190 The hydraulic capacitance of the stem was calculated as the derivative of the water release curve191 (Steppe *et al.*, 2006):

192
$$C_S = \frac{dW}{d\Psi}$$
 Eqn. 2

193 where dW is the variation in water content in the storage compartment (g h⁻¹) and d Ψ the 194 corresponding variation in Ψ (MPa h⁻¹). In this study, the cumulative water (W) release curve was 195 defined by a logarithmic equation of similar shape to those previously reported (e.g. Meinzer *et al.*, 196 2003, 2009; McCulloh *et al.*, 2014):

197
$$W = -\log_{w_1}(w_2\Psi + 1)$$
 Eqn. 3

198 where w_1 and w_2 are the parameters defining the shape of the water release curve. The derived form 199 of Eqn. 3 results in an inverse equation between C_s and Ψ_{PD} :

200
$$C_S = \frac{1}{(c_1 \Psi_{PD} + c_2)}$$
 Eqn. 4

where $c_1 (g^{-1})$ and $c_2 (MPa g^{-1})$ are the proportionality parameters dependent on plant properties, which are related to the parameters defining the water release curve (Eqn. 3) as follows: $w_1 = e^{c_1}$, and $w_2 = \frac{\ln(w_1)}{c_2}$. Note that the purpose of this study is to evaluate seasonality in R_x and C_s . Therefore, R_x and C_s in this model fluctuates on a daily basis with Ψ_{PD} , so that both are assumed constant within 24 h periods as diel variability in R_x and C_s is expected to be comparatively negligible (see Baert *et al.*, 2015). Four models were calibrated for each tree: [1] R_x and C_s were assumed to be constant (the simplest framework, used for model calibration of R_x and C_s), [2] R_x was allowed to vary and C_s was assumed to be constant (model calibration of r_1 , r_2 and C_s), [3] C_s was allowed to vary and R_x was assumed to be constant (model calibration of R_x , c_1 and c_2), and [4] both R_x and C_s were allowed to vary (model calibration of r_1 , r_2 , c_1 and c_2). The resistance to radial flow between xylem and storage compartment (R_s) was also calibrated in each model.

213 2.3.2 Model simulation, calibration, and identifiability analyses

214 Model simulations, calibrations and identifiability analyses were performed using the plant modelling 215 software PhytoSim (version 2.1, Phyto-IT, Mariakerke, Belgium). Simulations were conducted with a fourth order variable step size solver of an accuracy of 10^{-6} and a maximum step size of 1 h. 216 217 Calibrations were done using the simplex method to minimize the weighted sum of squared errors (SSE) for ΔD and Ψ_X . Identifiability analyses were performed to check whether the subset of model 218 219 parameters to calibrate was not correlated and sensitive enough, and thus was identifiable (De Pauw 220 et al., 2008). A collinearity index (CI) above 15 indicated an unidentifiable subset of parameters. 221 Values of non-calibrated model parameters were directly measured or assigned from literature 222 (Table S1 in supplementary material).

223 Predawn water potential and F_{STEM} were used as model inputs, and ΔD and Ψ_X were used for 224 calibration purposes. The best model was selected using the final predicted error (FPE) criteria 225 (Steppe *et al.*, 2006):

$$226 FPE = \frac{SSE}{N} + \frac{2pSSE}{(N-p)N} Eqn. 5$$

where SSE is the weighted sum of squared errors for ΔD and Ψ_{x} , *N* is the number of observations, and *p* the number of calibrated parameters. The first term of the FPE evaluates the goodness of fit between measured and simulated data, whereas the second term penalizes over-parameterized models. Thus, the smaller the FPE value, the better the model. Because rain events and tree trembling resulted in irregular signals recorded by the automatic band dendrometers, data was manually inspected to select a set of days that displayed reliable diel patterns, i.e., smooth morning shrinkage and afternoon swelling. As the number of ΔD observations after manual inspection differed among trees, FPE values also differed. To remove any effect associated to the number of observations, values of FPE were normalized relative to the simplest framework (constant R_x and C_s) for each tree.

237 Models were calibrated under wet and dry conditions. As stem growth during the summer season is 238 limited by soil water availability in the surveyed site (Lempereur et al., 2015), wet and dry periods 239 were defined according to growing or non-growing conditions, respectively. Periods that cover two 240 consecutive midday Ψ_{LEAF} measurements were initially considered for model calibration: DOYs 113-241 177 were selected for the wet period (spring and early summer) and DOYs 207-235 for the dry period 242 (late summer). Inaccurate simulations were initially obtained during the wet period and further 243 attempts to improve simulations were tested. First, the stem growth curve was adjusted to a 244 Gompertz-shaped curve (Winsor, 1932) to smooth large fluctuations registered by the band dendrometers (Fig. 1D); and second, a shorter time period around a single Ψ_{LEAF} measurement 245 246 campaign (DOY 176, early summer) was additionally examined.

247 To calibrate the models, midday Ψ_X was inferred from midday Ψ_{LEAF} measurements. Under dry conditions, measurements of midday Ψ_{LEAF} could be used as a surrogate of midday Ψ_{X} , because of the 248 249 strong stomatal limitation observed in the monitored trees (see Fig. 3 in Limousin et al., 2010b) 250 which minimized the disequilibrium in water potential between xylem and leaves (Meinzer et al., 251 2009). In contrast, substantial disequilibrium between midday Ψ_{LEAF} and midday Ψ_{X} might occur 252 when water is not limiting, as has been observed in Q. ilex seedlings (Rodríguez-Calcerrada et al., 253 2017) and in Neotropical savanna trees (see Fig. 2 in Scholz et al., 2007). Under wet conditions, the 254 difference between midday and predawn Ψ_x ($\Delta \Psi_x$ = midday Ψ_x – predawn Ψ_x) was assumed as a 255 constant fraction of $\Delta \Psi_{LEAF}$ ($\Delta \Psi_{LEAF}$ = midday Ψ_{LEAF} – predawn Ψ_{LEAF}). The ratio $\Delta \Psi_{\chi}$ / $\Delta \Psi_{LEAF}$ was 256 obtained from measurements performed in Q. ilex seedlings ($\Delta \Psi_X / \Delta \Psi_{LEAF} = 0.342$; Fig. S1 in

supplementary material), in which leaves were covered with aluminium foil for one hour to measure Ψ_{x} . Midday Ψ_{x} was therefore estimated as a function of Ψ_{PD} and $\Delta\Psi_{LEAF}$ (midday $\Psi_{x} = \Psi_{PD} + 0.342 *$ $\Delta\Psi_{LEAF}$). By using this approximation of Ψ_{x} , we made the assumptions that leaf hydraulic resistance was a constant fraction of the tree hydraulic resistance independently of tree size (Sack *et al.*, 2003), that the water potential difference between leaves and stem depended mainly on leaf transpiration, and that the Ψ_{x} difference between the trunk and the branches was negligible.

263 2.4 Stem water refilling measurements

264 Stem water refilling was estimated by integrating sap flow over intense rain events at the end of 265 summer drought. We only considered short (< 4 hours) and heavy (> 20 mm) rainfall events occurring 266 at night or in the late evening to ensure that recorded sap flow could be attributed to stem water 267 refilling and not to leaf transpiration (Betsch et al., 2011), and to avoid rainfall events that resulted in 268 slow refilling extending beyond night-time. Sap flow was integrated along the rain event and 269 following night-time hours to estimate the volume of water refilled. Stem water refilling was then 270 divided by the corresponding shift in Ψ_{PD} measured before and after the rain event to estimate C_S 271 (Eqn. 2) and compare it with values obtained from model simulations. Available measurements of Ψ_{PD} obtained less than one week before and after the rainfall event were necessary to calculate C_s. 272 273 As the first heavy rain in 2009 did not meet these requirements, different years were inspected and suitable rain events were found in 2006 and 2007 to estimate Cs. TREE4 was excluded from this 274 275 analysis, as it was not monitored in 2006 and 2007. However, eighteen Q. ilex trees located in the 276 study site and equipped with thermal dissipation probes were additionally included.

277 2.5 Data analyses

To compare model performance (i.e. normalized FPE) among the four tested models and the two surveyed periods, Tukey's multiple comparison tests were performed using the *TukeyHSD* function in the R software (version 3.2.3). The best model was then selected to obtain R_X and C_S along the gradient of Ψ_{PD} on a per-tree basis. To test whether F_{STEM} and radial water flow (f_S) varied with Ψ_{PD} ,

282 mixed models were adjusted using the Ime function in the nlme library, in which stem was considered as a random factor (n = 6). As the model output for C_s refers to the whole tree, C_s was 283 284 standardized per unit of storage volume. The storage volume was estimated as the product of stem height by stem basal area subtracting the xylem compartment. The integrated root-to-leaf hydraulic 285 conductance was calculated as the inverse of the integrated root-to-leaf hydraulic resistance (K_x = 286 $1/R_{x}$, g MPa⁻¹ h⁻¹). Predawn water potential causing 50% loss of K_x (Ψ_{50}) was obtained following Baert 287 288 et al. (2015). To obtain the mean curve and confidence intervals of C_s, cumulative water release, and 289 integrated root-to-leaf R_X and K_X along the gradient of Ψ_{PD} , uncertainty analyses were performed in 290 PhytoSim using the averaged parameters among the six studied trees yielded by the best model. All 291 values presented in the text are means ± SE.

292 3 Results

Averaged among the six surveyed stems and across the whole year, daily sap flow was 4.11 ± 0.81 kg day⁻¹ (Fig. 1C, Table 1), and mean annual diameter increment was 0.53 ± 0.20 mm year⁻¹ (Fig. 1D, Table 1). During spring and early summer (DOYs 113-177), average temperature was $18.2 \,^{\circ}$ C and accumulated rainfall 107.2 mm. Late summer was hot and dry, with an average temperature of 25.2 °C and an accumulated rainfall of 11.8 mm during the dry modelled period (DOYs 207-235). The lowest Ψ_{LEAF} was measured at the end of this period, when it reached mean values of -3.3 MPa at predawn and -3.9 MPa at midday (Fig. 1B).

Four models with constant or variable R_x and C_s were adjusted per tree and period to simulate ΔD and Ψ_x over time. A consistent pattern was observed under wet (Fig. 2A) and dry (Fig. 2B) conditions. Relative to the simplest model (constant R_x and C_s), the normalized FPE was not reduced when R_x alone was allowed to vary (P > 0.1). In contrast, the normalized FPE was reduced (P < 0.001) when C_s was allowed to vary with Ψ_{PD} . The model with variable R_x and C_s showed the lowest normalized FPE, although its value did not differ significantly from that obtained with constant R_x and variable C_s (P > 0.1). Therefore, calibration of the model with a variable C_s was the main improvement required to 307 accurately simulate ΔD and Ψ_x . Only data yielded by the best model (variable R_x and C_s) is shown 308 hereafter.

Models were calibrated under wet and dry conditions. Only TREE5 was not modelled during the wet 309 310 season due to the inconsistent dendrometer signal at the time of Ψ_{LEAF} measurement. Because of 311 concurrent stem growth, inaccurate simulations of ΔD were initially obtained during the wet period when considering long temporal spans (DOYs 113-177; data not shown). Shorter temporal spans of 3-312 313 4 days resulted in realistic simulations of Ψ_{x} and ΔD (Fig. 3A-C, FPE = 6.04 ± 1.90). The length of the 314 simulation period was not an issue under dry conditions when stem growth was impeded, and 315 accurate simulations were obtained for every tree throughout the one-month simulated period (Fig. 316 3D-F, FPE = 7.71 ± 2.11). During the wet season, cell turgor pressure at night-time was higher than the turgor threshold for cell wall yielding ($\Psi_s^P > \Gamma$, Fig. 3A) leading to irreversible stem growth (Fig. 317 318 3B). During the dry season, soil drying progressively reduced Ψ_x , Ψ_s and cell osmotic potential, which 319 explained the rather constant pattern of cell turgor pressure, which was below the turgor threshold for cell wall yielding ($\Psi_s^P < \Gamma$, Fig. 3D), thus impeding irreversible stem growth (Fig. 3E). Morning stem 320 321 shrinkage and afternoon stem swelling (Fig. 3B, 3E) were caused by the radial water flow between 322 xylem and storage compartments (f_s, Fig. 3C, 3F).

323 Daily F_{STEM} was directly related to Ψ_{PD} in every surveyed stem (P < 0.01, Fig. 4A). Averaged among the six stems, F_{STEM} decreased from 7.50 ± 0.83 kg day⁻¹ during the wet period (Ψ_{PD} = -1.0 MPa) to 1.46 ± 324 0.81 kg day⁻¹ at the end of the dry period (Ψ_{PD} = -3.3 MPa, P < 0.001). The decrease in daily stem 325 326 water release from the storage to the xylem compartment (daily sum of negative f_{s_i} hereafter daily $|f_s|$, in kg day⁻¹) with Ψ_{PD} was significant in only half of the surveyed trees (P < 0.05, Fig. 4B) and 327 became non-significant when pooling trees across a range of Ψ_{PD} from -1.0 to -3.3 MPa (P = 0.15). 328 Considering the dry period only, daily $|f_s|$ significantly decreased with Ψ_{PD} (P < 0.001) from 0.13 ± 329 0.03 to 0.10 ± 0.03 kg day⁻¹ for a corresponding reduction in Ψ_{PD} of 1.3 MPa (from -2.0 to -3.3 MPa). 330 331 Across the year, daily sap flow was reduced to a greater extent than daily $|f_s|$ as the soil dried out. Hence, the daily contribution of $|f_s|$ to F_{STEM} increased with drought severity (P < 0.001) from 2.0 ± 0.9 % to 5.1 ± 0.9 % when Ψ_{PD} decreased from -1.0 to -3.3 MPa (Fig. 4C).

Stem hydraulic capacitance decreased with drought stress. Mean C_s on a storage volume basis was 334 61.69 ± 6.30 kg MPa⁻¹ m⁻³ under wet conditions (Table 2) and reached lowest values of 24.93 ± 4.14 335 kg MPa⁻¹ m⁻³ at the end of the summer drought (Table 3). Fig. 5A illustrates the mean cumulative 336 release of water from storage compartments and the change in Cs at the tree level obtained in the 337 338 dry period and extrapolated to a wider range of Ψ_{PD} . Hydraulic capacitance obtained from model calibration during the wet period ($C_s = 314.51 \pm 38.83$ g MPa⁻¹ tree⁻¹) was underestimated by the C_s 339 340 curve extrapolated from the dry period. Similarly, Fig. 5B displays mean R_x and K_x curves obtained in 341 the dry period. The vulnerability curve of root-to-leaf hydraulic conductance obtained from the dry 342 period showed a mean Ψ_{50} value of -2.67 ± 0.23 MPa (Table 3). The R_x value obtained from direct model calibration under wet conditions (5.01 \pm 0.45 \times 10⁻⁴ MPa h g⁻¹, Table 2) was overestimated by 343 the R_x curve extrapolated from summer drought. 344

Two rain events were used to independently estimate C_s from stem water refilling. In 2006, 24 mm of rainfall were registered during the night of DOY 228 to 229, whereas in 2007, a stronger rainfall of 75.5 mm occurred in the night of DOY 261 to 262. The corresponding mean increase in Ψ_{PD} was 2.6 and 2.9 MPa for 2006 and 2007, respectively. Stem water refilling and C_s on a tree basis were exponentially related to stem size across the 23 trees examined (P < 0.001; Fig. 6). Average stem water refilling and C_s among the five trees monitored in both approaches were 1134 ± 149 g tree⁻¹ and 414 ± 45 g MPa⁻¹ tree⁻¹, respectively.

352 4 Discussion

353 4.1 The importance of a variable hydraulic capacitance in tree modelling

Hydraulic capacitance is commonly measured as the slope of the initial and nearly linear portion of the curve between the cumulative water release and water potential (Meinzer *et al.*, 2003, 2008; Barnard *et al.*, 2011; McCulloh *et al.*, 2014). These estimates of C_s are therefore obtained within the 357 range of Ψ_x when plants are not subjected to drought stress. Notwithstanding, C_s varies seasonally as water storage refilling is limited by soil drying (Verbeeck et al., 2007; Scholz et al., 2008; Steppe et al., 358 2008b; Kocher et al., 2013; Matheny et al., 2015). Progressive decoupling between daily capacitive 359 water discharge and daily water refilling leads to water reserves depletion, and accordingly, a net 360 361 reduction in stem diameter is commonly observed during the dry season (Fig. 3E; Zweifel et al., 2000; 362 Lempereur et al., 2015). Progressive depletion of water reservoirs should be incorporated in process-363 based hydraulic models by the implementation of a direct relationship between C_s and soil water 364 availability. However, to the best of our knowledge, no mechanistic model has yet considered 365 drought-induced variability in C_s to model tree hydraulic functioning. Furthermore, and unexpectedly, 366 considering the variation of C_s with Ψ_{PD} was also found to result in more accurate simulations of Ψ_x 367 and ΔD during the wet period. In contrast to previous studies using this model in which C_s was 368 assumed constant under well-watered regimes and stable soil water content (e.g. Steppe et al., 2006, 369 2008a; De Schepper & Steppe, 2010), considering a variable C_s was here necessary to simulate the 370 increase in turgor that yielded irreversible cell wall extension. Assuming a constant Cs in our study 371 resulted in a progressive reduction of maximum daily turgor pressure that impeded stem growth 372 (simulations not shown) as Ψ_{PD} slightly declined during this "wet" period (Fig. 3A). Consequently, 373 under both wet and dry conditions, assumptions of constant C_s may partially explain why tree models 374 fail to reproduce variations in diameter and Ψ_x in environments where soil water availability 375 fluctuates. We suggest that to better predict and understand tree hydraulic functioning and the risk of hydraulic failure in dry regions, it is necessary to take into account the dynamic nature of C_s. 376

Because C_s is commonly measured under moist conditions, estimates of C_s on a storage volume basis in early summer (62 kg m⁻³ MPa⁻¹, Table 2) might be more appropriate for literature comparison. Hydraulic capacitance of *Q. ilex* at this time of year was consistent with the reported range for evergreen sclerophyll species (6-102 kg m⁻³ MPa⁻¹, Richards et al. 2014) and lower than the ones for tropical species (70-420 kg m⁻³ MPa⁻¹, Meinzer et al. 2003, 2009) and conifers (107-886 kg m⁻³ MPa⁻¹, Barnard et al. 2011, McCulloh et al. 2014). Nevertheless, neglecting the xylem tissues as capacitive

water sources might lead to underestimation of the overall hydraulic capacitance of Q. ilex stems in 383 our study (see below). Hydraulic capacitance decreased across the season from 62 to 25 kg m⁻³ MPa⁻¹ 384 (from DOY 176 to 235, respectively). The 60% reduction in C_s illustrates the importance of 385 386 implementing variable C_s in mechanistic models to accurately simulate tree water status and 387 diameter variations. Our modelling approach further allowed estimation of the daily contribution of 388 internal water storage to total daily sap flow ($|f_S| / F_{STEM}$) as a function of Ψ_{PD} . The average $|f_S| / F_{STEM}$ F_{STEM} ratio ranged between 2% in early summer and 5% at the end of summer drought when Ψ_{PD} 389 390 reached mean values of – 3.3 MPa (Fig. 4C). This ratio is at the lower end of observations made in 391 other species that may reach up to 19% when only elastic tissues are considered (see Table 3 in 392 Betsch et al., 2011). The low reliance on stored water to maintain transpiration rates in Q. ilex might 393 be related to the wood features of this species with relatively high wood density and small vessel size 394 (Limousin et al., 2010a). These characteristics make trees more cavitation-resistant to xylem tension, 395 an adaptation which seems to be related to a limited capacity to reduce xylem tension via radial 396 water release (Meinzer et al., 2008, 2009; Richards et al., 2014). This trade-off also explains that Cs of 397 Q. ilex is at the lower end of reported values (see Fig. 5 in Meinzer et al. 2009 for comparison). Despite low $\left| f_{S} \right|$ / F_{STEM} ratios, the reliance on stored water increased with drought stress due to a 398 399 more pronounced reduction in daily F_{STEM} compared to daily |f_s|. A similar pattern was also noticed 400 in Quercus robur L., which used stored water primarily when subjected to drought stress (Matheny et 401 al., 2015). These observations suggest greater relevance of stem water reservoirs to maintain 402 transpiration rates and tree hydraulic integrity in future drier climates (see Tyree & Ewers 1991; and 403 Bréda et al. 2006).

404 4.2 Model limitations

Two limitations related to the model structure and assumptions were detected during this study. First, accurate simulations of diameter variations during the wet period were restricted to time frames of 3-4 days. Beyond this short time interval, diameter simulations progressively deviated from measured values. During dry conditions, however, the length of the model period was not an issue 409 because irreversible stem growth was prevented by soil water limitation (Lempereur et al., 2015). Any diameter variation during summer drought could be uniquely ascribed to radial water flow 410 411 causing elastic stem shrinkage and swelling. In contrast, during the wet period when irreversible 412 growth occurred, the carbon status of the plant is a factor involved in growth, for example via 413 osmotic regulation of cell turgor and elongation (Lockhart, 1965; Daudet et al., 2005). The lack of 414 carbon-related equations in our water-based model describing sugar transport and/or carbon 415 allocation to growth could explain inaccurate simulations when the modelled period extended 416 beyond 3-4 days. Accordingly, the generally prescribed time frame for this model ranges from one 417 day to two weeks (Steppe et al., 2006, 2008b). More sophisticated models integrating water and 418 carbon transport processes should be further developed to simulate irreversible stem growth on a seasonal basis (De Schepper & Steppe, 2010; Mencuccini et al., 2015; Steppe et al., 2015a). 419

420 Second, the model is theoretically designed to estimate C_s only for outer tissues and we ignore the 421 amount of water released by the xylem compartment. The contribution of the xylem to whole stem 422 diameter variations is expected to be minor (Zweifel et al., 2000; Steppe & Lemeur, 2004; Steppe et 423 al., 2006), and our model therefore assumes the xylem as a rigid compartment and outer tissues – 424 namely cambium, phloem, and phelloderm – as an elastic storage compartment responsible for diel 425 shrinkage and swelling. Nevertheless, the amount of water released for a given change in volume is 426 higher in the xylem than in the outer tissues; about 3.5 times higher in the case of savanna trees, 427 which results in a greater capacitance of the xylem compartment (Scholz et al., 2007, 2008). Higher 428 capacitance of the xylem can be ascribed to both elastic living parenchyma and the capacitive effect 429 of cavitated conduits (Tyree & Ewers, 1991; Hölttä et al., 2009; Richards et al., 2014). Thus, water 430 release from the xylem could be important in large trees with a high proportion of sapwood and 431 lumen volume (Waring et al., 1979; Hölttä et al., 2009; Betsch et al., 2011) or with large and 432 numerous sapwood parenchyma rays such as Q. ilex. Models considering the capacitive effect of 433 cavitation (Hölttä et al., 2009) and the xylem as an elastic compartment with a distinct elastic bulk 434 modulus and hydraulic capacitance (Perämäki et al., 2005) would be necessary to further disentangle

the contribution of elastic outer tissues and xylem parenchyma, and inelastic cavitated conduits tothe overall capacitive discharge of water to the transpiration stream.

437 **4.3** Simulated stem water release curves, root–to–leaf vulnerability curves and model validation

Simulations performed under dry conditions misestimated both C_S and R_x when extrapolated to a wider range of Ψ_{PD} during wet conditions, and values obtained for well-watered conditions were also necessary to realistically describe the C_S and R_x curves over the entire Ψ_{PD} range (Fig. 5). This observation denotes that any extrapolation beyond the surveyed range of Ψ_{PD} must be taken with caution. More frequent measurements of Ψ_{LEAF} (or Ψ_x) would be necessary to re-calibrate model parameters at a higher temporal resolution (Steppe *et al.*, 2008b) and obtain a more accurate evolution of C_S and R_x across a wider range of Ψ_{PD} .

445 Estimates of stem water refilling following first heavy rains at the end of the drought period and the 446 vulnerability curves obtained by measurements at the organ scale were compared to model simulations. At the end of summer drought, the modelled cumulative water release averaged 683 g 447 tree⁻¹ at a Ψ_{PD} of -3.33 MPa (Fig. 5A), which is 60% of that estimated from the refilling calculations 448 (1134 g tree⁻¹ for a corresponding increase in Ψ_{PD} of 2.75 MPa, Fig. 6A). Likewise, mean C_s modelled 449 across the range of surveyed conditions (from 103 to 314 g MPa⁻¹ tree⁻¹, Fig. 5A) was lower than that 450 estimated following heavy rains (414 g MPa⁻¹ tree⁻¹, Fig. 6B). Inaccurate assumptions to estimate 451 452 stem storage capacity and C_s using both approaches may account for this difference. First, C_s could 453 be overestimated from water refilling calculations because the corresponding water potential 454 increase was measured several days apart from the refilling event, and was therefore slightly 455 underestimated. Besides, water refilling of branches and leaves incorrectly attributed to the stem 456 may overestimate the actual stem storage capacity. Second, C_s might be underestimated from model 457 simulations due to the water release from xylem tissues (Scholz et al., 2008; Hölttä et al., 2009) 458 undetected by our model. Models that integrate the hydraulic capacitance of the xylem compartment, continuous in vivo measurements of wood water content using frequency domain 459

460 reflectometry (Matheny *et al.*, 2015), or destructive sampling to obtain stem moisture release curves 461 with psychrometers (Meinzer *et al.*, 2003) might be complementary approaches to more accurately 462 estimate the overall hydraulic capacitance of the stem. Likewise, direct measurements of Ψ_x would 463 result in more accurate estimates of C_s than the simulated here, in which Ψ_x was inferred from Ψ_{LEAF} 464 measurements.

465 On the other hand, variation in R_x as a function of drought stress affected to a lesser extent the 466 model performance. The simulated vulnerability curve along the root-to-leaf continuum exhibited 467 reasonable agreement with measurements made at the organ scale at the same site. The mean 468 simulated Ψ_{50} was -2.67 MPa (Table 3). Estimates of Ψ_{50} in excised branches and roots of *Q. ilex* trees 469 located at the same site averaged -3.88 and -2.39 MPa, respectively, using the air injection technique 470 after flushing native embolism (Limousin et al., 2010a), and -4.7 MPa in branches using the bench 471 drying technique (Martin-StPaul et al. 2014). Vulnerability to drought in the root-to-leaf continuum 472 is determined to the greatest extent by the most vulnerable node along this hydraulic pathway (Baert 473 et al., 2015). In this particular case, roots might be the major constrain to water flow along the root-474 to-leaf continuum, followed by stems and branches (Tyree & Ewers, 1991; Sperry & Love, 2015). 475 Therefore, the integrated Ψ_{50} (-2.67 MPa) might primarily reflect the hydraulic vulnerability of roots. 476 This alternative approach to generate integrated root-to-leaf vulnerability curves might be useful to 477 describe the hydraulic functioning of the whole tree while avoiding to separately measure multiple 478 hydraulic resistances (Baert et al., 2015), which might be controversial due to the strong variability in 479 hydraulic conductance ascribed to methodological issues (Cochard & Delzon, 2013; Martin-StPaul et 480 al., 2014).

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Table 1. Diameter at breast height (DBH), tree height, accumulated diameter increment and mean

629 daily sap flow during 2009 for the six monitored *Quercus ilex* trees.

	DBH	Height	Annual diameter increment	Mean sap flow	
	(cm)	(m)	(mm year ⁻¹)	(kg day ⁻¹)	
TREE1	9.55	5.3	0.25	2.55	
TREE2	11.05	5.0	0.16	3.00	
TREE3	10.70	5.0	0.51	5.87	
TREE4	13.20	5.6	1.21	7.32	
TREE5	10.05	5.2	-0.10	2.90	
TREE6	12.25	4.5	1.15	3.00	

Tree DBH measured at the beginning of the 2009 growing season

632**Table 2.** Hydraulic resistance to radial flow between the xylem and the storage compartment (R_s),633hydraulic resistance of the root-to-leaf segment (R_x), and stem hydraulic capacitance (C_s) obtained634from the mechanistic water flow and storage model describing the hydraulic functioning of *Quercus*635*ilex* trees during the wet season when stem growth occurred.

	R _s	R _X	Cs	
	(MPa h g ⁻¹)	(MPa h g⁻¹)		
	10 ⁻²	10 ⁻⁴	(kg MPa ⁻¹ m ⁻³)	
		4.59	64.02	
TREE1	0.97	[4.59 - 4.59]	[54.66 – 72.22]	
	1.41	5.72	50.06	
TREE2		[5.72 -5.72]	[45.03 – 54.79]	
	0.93	4.59	86.07	
TREE3		[4.59 -4.59]	[73.33 – 98.28]	
	0.53	3.65	61.38	
TREE4		[3.62 -3.69]	[54.98 – 66.94]	
TREE5 ¹	NA	NA	NA	
TREE6	1.15	6.49	46.91	
		[6.38 – 6.62]	[41.67 – 52.69]	
mean	1.00	5.01	61.69	
(SE)	(0.13)	(0.45)	(6.30)	

 R_s was assumed constant whereas R_x and C_s were allowed to vary with predawn water potential (Eqn. 1 and Eqn. 4, respectively). The modelled period lasted 3-4 days and included DOY176, when leaf water potential was measured. Mean values of R_x and C_s on a storage volume basis are shown; minimum and maximum values for this period are indicated in square brackets.

640 ¹ TREE5 was not modelled due to an inconsistent dendrometer signal.

Table 3. Calibrated parameters used in the mechanistic water flow and storage model describing the hydraulic functioning of *Quercus ilex* trees during summer drought when stem growth was impeded. The hydraulic resistance (R_x) and hydraulic capacitance (C_s) were allowed to vary with predawn water potential (Ψ_{PD}). Estimates of C_s and the Ψ_{50} from the vulnerability curve were obtained from model simulations.

	Calibrated parameters ¹				C _s ²		Ψ_{50}^{3}	
	R _s	C ₁	C ₂	r ₁	r ₂	DOY208	DOY234	* 50
	(MPa h g⁻¹)	(g ⁻¹)	(MPa g⁻¹)	(MPa h g ⁻¹)	(MPa⁻²)	(kg MPa ⁻¹ m ⁻³)		
	10 ⁻²	10 ⁻³	10 ⁻³	10 ⁻³	10 ⁻¹			(MPa)
TREE1	1.95	-3.07	2.68	0.99	1.29	26.52	18.48	-2.32
TREE2	1.73	-2.54	2.01	1.68	0.67	28.91	19.84	-3.21
TREE3	2.30	-2.33	2.78	1.26	1.53	31.75	23.34	-2.13
TREE4	0.53	-0.73	1.11	0.77	0.91	56.30	45.30	-2.76
TREE5	1.31	-2.99	1.20	3.15	1.55	37.43	22.66	-2.12
TREE6	1.88	-2.28	2.34	3.67	0.58	28.04	19.96	-3.46
mean	1.62	-2.32	2.02	1.92	1.09	34.82	24.93	-2.67
(SE)	(0.25)	(0.35)	(0.29)	(0.49)	(0.17)	(4.57)	(4.14)	(0.23)

¹ Five parameters were calibrated: the proportionality parameters c_1 and c_2 defining C_s (Eqn. 4), the proportionality parameters r_1 and r_2 defining R_x (Eqn. 1), and the radial hydraulic resistance between the xylem and the storage compartment (R_s).

² C_s was estimated for two dates when Ψ_{PD} was measured (DOYs 208 and 234) and calculated on a storage volume basis.

651 ³ Ψ_{50} is the Ψ_{PD} causing 50% loss of maximum hydraulic conductance along the integrated 652 root-to-leaf continuum.

Figure 1. Daily air temperature and precipitation (A), soil water storage and predawn and midday leaf water potential (means ± SE; B), daily sap flow (C), and daily stem diameter variations (D) during the year 2009. Ecophysiological measurements were performed on six *Quercus ilex* trees of the experimental site.



659 Curves of accumulated diameter increment were smoothed according to the Gompertz's equation 660 (dashed lines). Diel variations in diameter are not shown for clarity.

Figure 2. Normalized final prediction error (FPE) of four tested models with constant or variable
 hydraulic resistance (R_x) and capacitance (C_s) to compare model performance. Models were used to
 simulate hydraulic functioning of *Quercus ilex* trees under wet (A) and dry (B) conditions.



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and penalizes over-parameterized models. Low FPE values indicate better model performance.

667 Values of FPE were normalized relative to the model with constant R_X and C_S to remove inter-stem

variability associated to the number of observations. Normalized FPE was averaged among six trees.

669 Different letters show significant differences (P < 0.05).

Figure 3. Measured and simulated water potentials (A, D), diameter variations (B, E) and water flows (C, F) in *Quercus ilex* trees during the wet (A-C) and the dry (D-F) season. Predawn water potential (Ψ_{PD}) and sap flow (F_{STEM}) (continuous black lines) were used as model inputs, whereas diameter variations and xylem water potential (Ψ_{x}) (black dots) were used for calibration purposes.







Figure 4. Variation in daily sap flow (A; F_{STEM}), daily stem water release (B; $|f_{\text{S}}|$), and the contribution of $|f_{\text{S}}|$ to F_{STEM} (C) in *Quercus ilex* trees along a gradient of predawn water potential (Ψ_{PD}).

Data from model simulations in early summer (wet period) and summer drought (dry period) are
 pooled. Only significant regressions are depicted (P < 0.05).

Figure 5. Hydraulic capacitance (C_s) and cumulative water released at the tree level (A), and hydraulic resistance (R_x) and conductance (K_x) in the root-to-leaf continuum (B) along a gradient of predawn water potential (Ψ_{PD}).



693 Calibrated parameters obtained from six *Quercus ilex* trees during the dry period (Table 3) were used 694 to estimate the mean (continuous line) and 95th and 5th percentile (dashed lines) curves of each 695 variable. The calibrated parameters were obtained from a mechanistic model in which R_X (Eqn. 1) 696 and C_S (Eqn. 4) were allowed to vary with Ψ_{PD} . Shaded areas indicate the modelled dry period, when 697 average Ψ_{PD} ranged between -1.98 and -3.33 MPa. The curves of C_S and R_X adjusted for long-term 698 (one-month) simulations of the dry period (in black) were improved by including values of the short-699 term (3-4 days) calibrations of the wet period (in red).

Figure 6. Stem water refilling (A) and hydraulic capacitance (C_s) (B) at the tree level estimated after the first heavy rain following the dry season. Two rain events registered in 2006 and 2007 (open and closed circles, respectively) met the minimum requirements to estimate stem storage capacity. Stem water refilling and C_s were estimated for a total of 23 *Quercus ilex* trees ranging in diameter at breast height (DBH) from 4 to 12.1 cm. Stem water refilling and C_s were exponentially related to tree DBH (Stem water refilling = $30.27 \times e^{(0.34 \times DBH)}$; $C_s = 15.05 \times e^{(0.31 \times DBH)}$; P < 0.001). Shaded areas indicate the range in DBH of trees additionally surveyed for modelling.

