## Novel kinetic model for the ethyl acetate synthesis by direct addition on a silicotungstic acid catalyst

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Ethyl acetate (EtAc) is an important organic chemical used in glues, surface coatings, thinners, paints, inks, nail polisher removal products and as solvent in physical and chemical processes [1, 2]. Among other processes, the gas phase direct addition of ethylene ( $C_2H_4$ ) and acetic acid (AcOH) catalyzed by a solid acid such as silicotungstic acid (STA) is the EtAc synthesis route that was commercialized by BP Chemicals and Showa Denko in the '90s [3, 4]. Due to the acidic nature of the catalyst and presence of water ( $H_2O$ ) in the AcOH feedstock, a variety of by-products, mainly ethanol (EtOH) and diethyl ether (DEE), other esters, alcohols, ethers, aldehydes, ketones and hydrocarbons are formed as well [5].

A kinetic model for the direct addition reaction focusing on the main products has been developed based on a simple mechanism (See Figure 1) in which six reacting components, i.e.  $C_2H_4$ , AcOH, H<sub>2</sub>O, EtAc, EtOH and DEE, are converted into each other via five reactions, denoted by r<sub>1</sub> to r<sub>5</sub>. r<sub>1</sub> to r<sub>3</sub> are direct additions of AcOH, H<sub>2</sub>O and EtOH to  $C_2H_4$  yielding EtAc, EtOH and DEE respectively, where r<sub>2</sub> is also referred to as the C<sub>2</sub>H<sub>4</sub> hydration, r<sub>4</sub> is the EtOH-AcOH esterification and r<sub>5</sub> is the EtOH condensation or dehydration to DEE.



**Figure 1:** Proposed reaction mechanism for the EtAc synthesis by direct addition.

The non-idealities of the gas phase, due to presence of AcOH, were captured by the Hayden and O'Connell equation of state for which the necessary parameters were retrieved from Aspen databases. Several kinetic models, based on different assumptions with respect to the adsorption of species, have been constructed for which the activation energies and adsorption enthalpies as adjustable parameters, were determined by regression to the experimental data with the aid of Athena Visual Studio. This software package was also used for statistical evaluation of the model and parameter estimates. In the optimized kinetic model, the rates of  $r_1$ ,  $r_2$  and  $r_4$  are described according to a Langmuir-Hinshelwood mechanism and the rates of  $r_3$  and  $r_5$  according to an Eley-Rideal type mechanism, in which the

adsorption of  $C_2H_4$ , AcOH,  $H_2O$ , EtAc and EtOH are included. The model has been improved by accounting for the dehydration of STA by  $H_2O$  and clustering of the STA protons with EtOH.



**Figure 2:** Effect of (<u>A</u>) T at 1.2 MPa and (<u>B</u>) P at 442 K and space time on  $x_{C_{2H_4}}$  at  $C_{2H_4}$ :AcOH:H<sub>2</sub>O:N<sub>2</sub> inlet molar flow ratio equal to 78.2:6.5:5.3:10.0. (•) T = 433 K, (•) T = 439 K, (•) T = 445 K, (•) T = 451 K, (•) T = 457 K, (•) T = 463 K, (▲) P = 0.8 MPa, (▲) P = 1.0 MPa, (▲) P = 1.2 MPa & (▲) P = 1.4 MPa. Symbols and lines represent experimental data points and model predictions respectively.

The kinetic model can accurately describe the effects of operating conditions, where the increase in  $C_2H_4$  conversion ( $x_{C_2H_4}$ ) with space time (W/F<sup>0</sup>), temperature (T) and  $C_2H_4$  concentration in the feed ( $y_{C_2H_4}^0$ ) and decrease with pressure (P), AcOH ( $y_{AcOH}^0$ ) and H<sub>2</sub>O feed concentration ( $y_{H_2O}^0$ ) are shown in Figure 2 and 3. Moreover, the model is capable to qualitatively predict the effects on selectivity to EtAc, EtOH and DEE. Furthermore, the kinetic model provides insights in how reaction rates are affected by the operating conditions and, hence, explains the observed trends in conversions and selectivities.



**Figure 3:** Effect of (<u>A</u>)  $y_{C2H4^0}$  with 6.5 mol% AcOH and 5.3 mol% H<sub>2</sub>O in the feed, (<u>B</u>)  $y_{AcOH^0}$  with 78.2 mol% C<sub>2</sub>H<sub>4</sub> and 5.3 mol% H<sub>2</sub>O in the feed) and (<u>C</u>)  $y_{H20^0}$  with 78.2 mol% C<sub>2</sub>H<sub>4</sub> and 6.5 mol% AcOH in the feed and space time on  $x_{C2H4}$  at T = 442 K and P = 1.2 MPa. (**a**)  $y_{C2H4^0} = 48.2$  mol%, (**b**)  $y_{C2H4^0} = 58.2$  mol%, (**c**)  $y_{C2H4^0} = 68.2$  mol%, (**c**)  $y_{C2H4^0} = 78.2$  mol%, (**c**)  $y_{C2H4^0} = 85.2$  mol%, (**c**)  $y_{AcOH^0} = 4.5$  mol%, (**c**)  $y_{AcOH^0} = 6.5$  mol%, (**c**)  $y_{AcOH^0} = 8.5$  mol%, (**c**)  $y_{AcOH^0} = 10.5$  mol%, (**c**)  $y_{H20^0} = 3.3$  mol%, (**c**)  $y_{H20^0} = 5.3$  mol%, (**c**)  $y_{H20^0} = 7.3$  mol% & (**c**)  $y_{H20^0} = 9.3$  mol%. Symbols and lines represent experimental data points and model predictions respectively.

The kinetic model that can simulate the effect of operating conditions on kinetics well, which is essential to consider predictions trustworthy. The model can be implemented in state-of-the-art process simulation software packages, such as Aspen Plus, to simulate the performance and identify better operating points for EtAc production plants that apply the direct addition technology. Hence, the kinetic model is a viable tool to optimize the performance of the production plants.

Keywords: ethyl acetate, direct addition, kinetic model, mechanism

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